# Predicting Tractive Performance using ZOZ Charts

Example: Determine the Drawbar Pull, Drawbar Power, and Actual Travel Speed for an International 5488 Tractor at maximum drawbar power poperating in 9<sup>th</sup> Gear, with full tractor ballast, semi-mounted plough in firm soil.

# **Preliminary Calc**

Before you can use the ZOZ, chart you need to determine the static rear axle force, no-load speed, and axle power available.

We will use the Nebraska Test #1441 to estimated these values for the drawbar tests on concrete. Preliminary Data, form Nebraska Test

 $\frac{\text{SRAF} = 7035 \text{ kg}, (15510 \text{ lb})}{\text{Drawbar Power} = 122.91 \text{ kW}, (164.82 \text{ Hp})}$ Speed = 8.48 km/h, (5.27 mph) Slip % = 3.52

## Calc zero slip speed

$TR = 100*(1 - S_a / S_o)$	
$S_o = S_a / (1 - TR/100)$	$S_o = S_a / (1 - TR/100)$
= 8.48/(1-3.52/100)	= 5.27/(1-3.52/100)
<u>= 8.79 km/hr</u>	<u>= 5.46 mph</u>

This no-load speed does not change, provide all calculations are in 9<sup>th</sup> gear, maximum power

# Finding the Axle Power for Tractor in 9th Gear

From Chart Read tractive efficiency (TE) to determine the axle power.

At 3.52 % Slip

Project line from 3.52% slip to left until hit the curve for concrete, the project up to the TE (Drawbar Power/Axle Power) axis and read TE (Yellow Line)  $\Rightarrow$  TE = 0.908

$TE = P_{db} / P_{a}$	$TE = P_{db} / P_{a}$
$\Rightarrow P_a = P_{db} / TE$	$\Rightarrow P_a = P_{db} / TE$
= 122.91 / 0.908	= 164.82 / 0.908
= 135.4  kW	= 181.5 Hp

The maximum axle power and no load speed will be constant for any calculations for <u>this</u> <u>tractor in 9<sup>th</sup> gear</u>, and any amount of tractor ballast (SRAF), slip or travel reduction, soil conditions or tillage tool.

# Using the ZOZ chart to determin Drawbar Pull etc.

Need to know the no-load speed & the ratio of SRAF/axle power

From preliminary calculations

No-load Speed	8.79 km/h,	(5.46 mph)
SRAF	7035 kg,	(15510 lb)
Axle Power	135.4 kW,	(181.5 Hp)

Calculate SRAF/axle power

$SRAF/P_a = SRAF(N) / P_a(kW)$	$SRAF/P_a = SRAF (lb) / P_a (Hp)$
= (7035*9.81) / 135.4	= 15,510 / 181.5
= 68,943 / 135.4	= 85.5 lb/Hp
= 509  N/kW	

Now ready to use the ZOZ chart starting at bottom with no-load speed

Start with  $S_o$  at Bottom left axis (5.46 mph) projecting a horizontal line to right (Red Line)  $\Rightarrow$  At the correct SRAF/Axle Power ratio in this case 85 lb/Hp show as blue line,

Project a vertical line up the upper right plot to intersect the correct soil/tillage tool combination To firm soil, semi-mount curve

Project to left a horizontal line to the correct soil type on the upper left plot in this case firm soil.

## From this line

The slip can be read directly off the left hand axis of the right upper plot  $\Rightarrow$  Slip 16%

To determine the Drawbar Pull project a line (red dashed line) down from the relevant family of soil/tillage tool (firm soil / semi mounted) curves to determine ration drawbar pull/SRAF

 $\Rightarrow$  drawbar pull/rear axle force = 0.65

To determine the Drawbar Power project a line (red line) up from the relevant soil type curve (firm soil) to detemine drawbar power/rear axle power (TE) from the upper axis

 $\Rightarrow$  Tractive Efficiency (0.725)

Calculate speed $S_a = S_o * (1 - TR/100)$	
$S_a = S_o * (1 - TR/100)$	$S_a = S_o * (1 - TR/100)$
= 8.79 * (1 - 16/100)	= 5.46 * (1 - 16/100)
= 7.4  km/h	= 4.6  mph
Calculate Drawbar Power $P_{db} = P_a * TE$	
$P_{db} = P_a * TE$	$P_{db} = P_a * TE$
= 135.4 * 0.725	= 181.5 * 0.725
= 98  kW	= 132 Hp
Calculate Drawbar Pull $F_{db} = SRAF * dt$	lrawbar pull/rear axle force
$F_{db} = SRAF * 0.65$	$F_{db} = SRAF * 0.65$
= 68,943 * 0.65	= 15,510 * 0.65
=44.8 kN	= 10081  lb.f

Check the above calculations: Note Power = Force \* Velocity Drawbar Force = 44.8 kN, 10081 lb.fVelocity = 7.4 km/h 4.6 mph Drawbar Power = 44.8 (kN) \* 7400 (m/h) / 3600 (s/h) = 92 kW (This is similar to that found above, error due to slight misreading of chart & small imperfections in relevant chart curves)

Drawbar Power = 10081(lb) \* 4.6(mph) \* 5280(ft/mile) / [60 (min/h) \* 33000({ft.lb/min}/Hp)] = 124 Hp (This is similar to that found above, error due to slight misreading of chart & small imperfections in relevant chart curves)

## **Determining Ballast**

Example: For the same tractor as in the last example, how much is required for the tector to operate with 20% slip on soft soil in 9<sup>th</sup> Gear

From Preliminary Calculation in the last example we know

zero slip speed=	8.79 km/hr,	5.46 mph
Axle Power=	135.4 kW,	181.5 Hp

# Require 20% Slip Using ZOZ Chart

Starting at the left axis of the top right plot

Start at 20% slip and project a horizontal line (green line) to the correct soil/tillage (soft soil /semi-mounted) tool curve.

Project a line down from this point in to lower right plot.

Now Start at left axis of of lower right plot with no load speed

Start with S<sub>o</sub> (5.46 mph) projecting a horizontal line to right (Dotted green line) until intersect with line above, to determine the required SRAF/axle power ratio Estimate the required ratio from sloping lines

⇒ Required SRAF/axle power ratio 860 N/Kw (metric)

⇒ Required SRAF/axle power ratio 140 lb/Hp

# Calculate Required SRAF (Know axle power from above)

Required SRAF = Axle Power \* Ratio= 135.4(kW)\*860(N/kW)= 181.5(Hp)\*140(lb/Hp)= 135.4(kW)\*860(N/kW)= 181.5(Hp)\*140(lb/Hp)= 116444(N)= 25,410 lb= 11,882 kg= 11,882 kg

Unballasted Weight (From Nebraska Tests) 5935 kg, 13085 lb

# **Calculate Ballast Required**

Ballast required = $11882 - 5935$	Ballast required= $25,410 - 13085$
<u>= 5947 kg</u>	<u>= 12,325 lb</u>

_	Pow	er	Crank	Fuel Co	insumption			Tem	perature	'F (°C)	-
	H (ky	P	shaft speed rpm	gal/br (Uh)	lb/hp.hr (kg/kW.h)	Hp.hr/j (kW.h/		Cooling medium	Air wet bulb	Air dry bulb	Barometer inch Hg (kPa)
				NIMUM	POWER	AND F	UEL	CONSI	UMPT	ION	
			Rate	d Engine	Speed—Tw	o Hours	(PTC	Speed-	-1005	rpm)	22270 (114)
	187.		2400	11.555 (43.740)	0.430 (0.262)	16.20 (3.19		190 (87.7)	61 (15.9)	75 (23.9)	28.873 (97.501)
	11.2.2.		VARVI	111111111	ER AND F					Hours	01010
	165	.46	2496	10.665	0.449	15.51		186	61	76	
_	(123.			(40.371)	(0.273)	(3.05	6)	(85.6)	(16.1)	(24.4)	
		.00	2614	3.446 (13.045)				176 (80.0)	60 (15.6)	74 (23.3)	
	84		2556	6.935	0.570	12.24		180	60	74	
	(63.		2000	(26.252)	(0.347)	(2.41		(82.2)	(15.6)	(23.3)	
	186		2400	11.517	0.430	16.23		189	60	75	
-	(139.		2590	(43.597) 5.184	(0.261)	(3.19		(87.2)	(15.8)	(23.9)	
	42		2000	(19.624)	(0.513)	(1.62		(80.6)	(15.6)		····· 
	125		2524	8.841	0.491	14.20		183	61	75	
Av	(93.		2530	(33.467)	(0.299)	(2.79	-	(83.9)	(16.1)	(23.9)	28.897
v	(75		2550	(29.394)	(0.326)	(2.56		(83.2)	(15.8)	(23.8)	(97.580)
				DRA	WBAR	PERF	OR	MAN	CE	11 1	
Po	wer	Drawb	ar Spee	d Crank-	Slip	Fuel Cor	sumpt	tion	Ten	np. *F (*C)	
1 (k	Ip W)	pull Ibs	mpł (km/k	shaft speed	% ga (l	(hr lb/h/h/h/h/h/h/h/h/h/h/h/h/h/h/h/h/h/h/h	p.hr H W.h)	Hp.hr/gal (kW.h/l)	Cool- ing	Air Air wet dry	Barom. inch Hy
_		(kN)		rpm					med	bulb bulb	(kPa)
163	3.44	1164			vailable Po 3.69 11.			urs 9th 14.16	(M3) Ga 187	55 67	28.915
(12	1.88)	(51.78	8) (8.4	7)	(43.	701) (0.	300)	(2.789)	(85.8)	(12.5) (19.2)	(97.642)
1.0/	0.87	879			Maximum 2.57 9.			Hours 9 13.15	th (M3) 182	Gear 56 66	28.951
	7.59)	(39.1-	- C.				322)	(2.591)	(83.4)	(13.6) (18.8)	
					Maximum				th (M3)		
	9.26 5.56)	586					522 378)	(2.209)	179 (81.7)	57 60 (13.9) (15.6)	28.945
					duced Engi		-Tw	o Hour		H1) Gear	
	9.32	586					470 286)	14.83 (2.921)	181 (82.8)	59 64 (15.0) (17.8)	28.895
[0	5.60)	(20.0)			JM POWI			http://www.	100000		())))))
	1 50	1004		022001010103				CIED		56 58	00.040
	1.52	1864			8.93	6th (L6)	Gear		181 (82.5)	(133) (14.4)	28.940 (97.726)
16	2.73	1600	1 3.8	1 2400	6.06	7th (M1)	Gear	a na	185	52 63	28.940
	1.35)	(71.10	C1 7 1	A.S. 199. 199.					(85.0)	(11.1) (17.2)	
	1.58	1353			4.35	8th (M2)	Gear		186 (85.3)	52 62 (11.1) (16.7)	28.940
16	1.82	1173	21. 22.		3.52	9th (M3)	Gear	6	186	53 60	28.970
(12	2.91)	(52.10	8) (8.4	8)				_	(85.6)	(11.7) (15.6)	
	4.43	987 (43.9-			2.92 1	0th (M4)	Gear		186 (85.6)	52 63 (11.1) (17.2)	28.940
	2.54	837			2.41 1	lth (M5)	Gear	6	188	52 64	28.940
10.5	1.21)	(37.2-							(86.4)	(11.1) (17.8,	(97.726
	0.12	698		**	1.80 1	2th (M6)	Gear		187	52 64 (11.1) (17.8)	28.940
(11)	9.40)	(31.00	8) (13.8			ITV IN	T 0+L	(119) (		(11.1) (17.0)	(97.720)
Cra	nksh	aft Sn	ed rpm		2398	2162	191		1682	1441	1204
-	-lbs		a tpin			13489	149		15838	15477	13385
	(ÅN					(60.00)	(66		(70.45)	(68.85)	(59.54)
Incr	ease	in Pul	1%		0	15	23	7	35	32	14
Pow	er—					69.56	165		152.46	127.90	93.55
Spe		(kW) Mph		(	122.91) (. 5.27	4.71	(123.	15	3.61	(95.37) 3.10	(69.76)
pe		(km/h)			5.27 (8.48)	4.71 (7.59)		15 68)	(5.81)	(4.99)	(4.22)
slin	Ct.				8 59	4 85		18	5.66	5 50	4.52

#### TABLE 16.2 Continued

4.35

5.18

5.66

5.50

3.52

Slip %

TRACTOR SO	dB(A)		
Maximum Avail	able Power—Two Hours		78.0
75% of Pull at M	faximum Power—Ten Hours	8	78.5
50% of Pull at M	faximum Power—Two Hour	\$	77.0
50% of Pull at R	teduced Engine Speed-Two	Hours	73.0
Bystander in 17	th (H5) gear		86.5
TIRES, BALLA Rear Tires Ballast	ST AND WEIGHT -No., size, ply & psi (kPa) -Liquid (each inner) -Test Equip. (each)	With Ballast Inner Two 20.8R38; 10; 12 ( Outer Two 20.8R38; 8; 12 (8 995 lb (452 kg) 109 lb (49 kg)	Without Ballast 85)Inner Two 20.8R38; 10; 12 (8 5)Outer Two 20.8R38; 8; 12 (85) None None
Front Tires Ballast	-No., size, ply & psi (kPa) -Test Equip (each) -Cast Iron (each)	Two 14L-16.1; 6; 28 (195) 130 lb (59 kg) 40 lb (18 kg)	Two 14L-16.1; 6; 28 (195) None None
Height of Drawb	wr.	21.5 in (545 mm)	21.5 in (545 mm)
Static Weight wi	th Operator—Rear —Front —Total	15510 lb (7035 kg) 4495 lb (2039 kg) 20005 lb (9074 kg)	13085 lb (5935 kg) 4155 lb (1885 kg) 17240 lb (7820 kg)
			4155 lb (1885 kg)

#### **Department of Agricultural Engineering**

Dates of Test: May 26 to June 8, 1982

Manufacturer: INTERNATIONAL HARVES-TER COMPANY, 401 North Michigan Avenue, Chicago, IL 60611

FUEL, OIL AND TIME: Fuel No. 2 Diesel Cetane No. 46.6 (rating taken from oil company's inspection data) Specific gravity converted to 60° (0° (15°)15°) 0.8375 Fuel weight 6.973 lbs/gal (0.836 kg/1) Oil SAE 30 API service classification CD/SE To motor 4.032 gal (15.262 l) Drained from motor 3.722 gal (14.088 l) Transmission and final drive lubricant 1.H. Hy-tran fluid Total time engine was operated 38.5 hours.

ENGINE: Make International Diesel Type six cylinder vertical with turbocharger and intercooler Serial No.  $467BT2U169510^{\bullet}$  Crankshaft lengthwise Rated rpm 2400 Bore and stroke  $4.30^{\circ} \times 5.35^{\circ}$  (109.2 mm  $\times$  135.9 mm) Compression ratio 16.3 to 1 Displacement 466 cu m (7636 ml) Starting system 12 volt Lubrication pressure Air cleaner two paper elements with aspirator Oil filter two full flow cartridges Oil cooler engine coolant heat exchanger for crańkcase oil, radiator for hydraulic and transmission oil Fuel filter two paper cartridges Muffler underhood Exhaust vertical Cooling medium temperature control one thermostat.

CHASSIS: Type standard with duals Serial No. 2590002U001019\* Tread width rear 64" (1625 mm) to 130" (3302 mm) front 62.5" (1588 mm) to 86.5" (2197 mm) Wheel base 111.6" (2835 mm) Center of gravity (without operator or ballast, with minimum tread, with fuel tank filled and tractor serviced for operation) Horizontal distance forward from center-line of rear wheels 26.9" (683 mm) Vertical distance above roadway 38.9" (988 mm) Horizontal distance from center of rear wheel tread 0" (0 mm) to the right/left Hydraulic control system direct engine drive Transmission selective gear fixed ratio with partial (2) range operator controlled powershift Advertised speeds mph (km/h) first 1.5 (2.4) second 1.8 (2.8) third 2.0 (3.2) fourth 2.4 (3.8) fifth 2.7 (4.4) sixth 3.2 (5.2) seventh 3.8 (6.1) eighth 4.5 (7.2) ninth 5.1 (8.3) tenth 6.0 (9.7) eleventh 7.0 (11.3) twelfth 8.2 (13.3) thirteenth 8.6 (13.8) fourteenth 10.1 (16.2) fifteenth 11.5 (18.5) sixteenth 13.6 (21.8) seventeenth 15.7 (25.3) eighteenth 18.5 (29.7) reverse 2.9 (4.6), 3.4 (5.4), 3.9 (6.2), 4.5 (7.3), 5.3 (8.5), 6.2 (9.9) Clutch wet multiple disc operated by foot pedal with hydraulic power assist Brakes wet multiple disc hydraulically power actuated and oper ated by two foot pedals which can be locked together Steering hydrostatic Turning radius (on concrete surface with brake applied) right 151.1" (3.84 m) left 151.1" (3.84 m) (on concrete surface without brake) right 199.5" (5.07 m) left 199.5" (5.07 m) Turning space diameter (on concrete surface with brake applied) right 316" (8.03 m) left 316" (8.03 m) (on concrete surface without brake) right 412" (10.47 m) left 412" (10.47 m) Power take-off 1005 rpm at 2400 engine rpm.

**REPAIRS and ADJUSTMENTS:** No repairs or adjustments.

**REMARKS:** All test results were determined from observed data obtained in accordance with SAE and ASAE test codes or official Nebraska test procedure. For the maximum power tests, the fuel temperature at the injection pump was maintained at 128°F (53.3°C). Seven gears were chosen between stability limit and 10 mph (16.1 km/h).

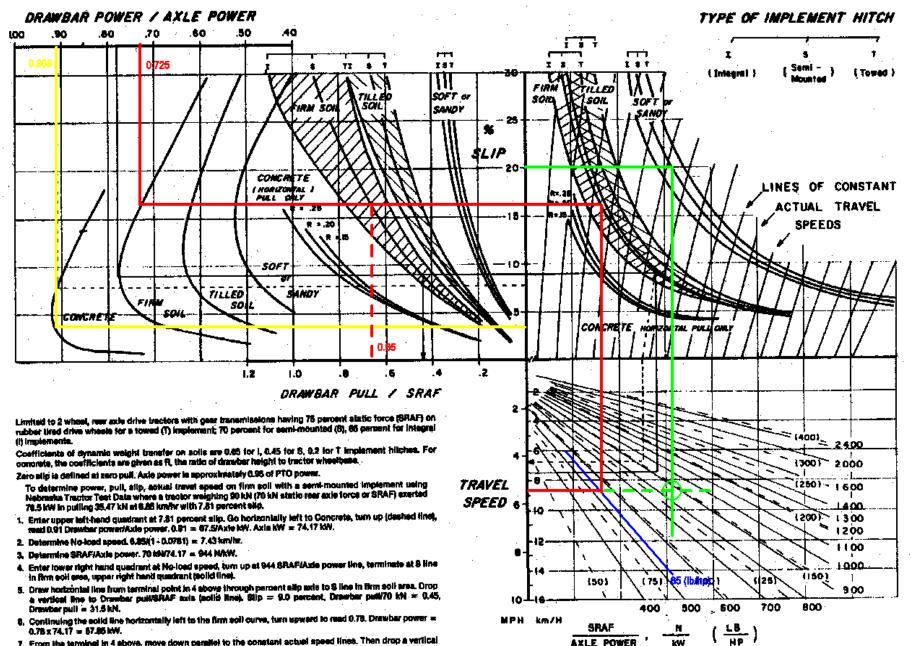
We, the undersigned, certify that this is a true and correct report of official Tractor Test 1441.

LOUIS I. LEVITICUS

Engineer-in-Charge K. VON BARGEN

> W. E. SPLINTER L. L. BASHFORD Board of Tractor Test Engineers

Source: Reprinted from University of Nebraska Tractor Test Laboratory, Report 1441.



7. From the terminal in 4 above, move down pamile) to the constant actual speed lines. Then drop a vertical to the 644 SRAF(Axle power burning line, go left, and read 6.8 km/hr actual speed (clashed line).

=FIGURE 16.9 Traction prediction chart (Reprinted from ASAE Data D230.4, Agricultural machinery management, revised December 1983)

AXLE POWER

k₩